

Dec 5, 2010

What is "detachment"?

Form of convective removal

convection = advection driven by  $\rho$  contrasts  
e.g. buoyancy forces ( $\rho$  is necessary)

$\Delta\rho$  can be compositional (chemical convection)  
or thermal, e.g.  $\frac{\Delta\rho}{\rho} = -\alpha \Delta T$  (thermal convection)

Magnitude of buoyancy forces

compositional

eclogite  $3400 \text{ kg/m}^3$

peridotite  $3300 \text{ kg/m}^3$

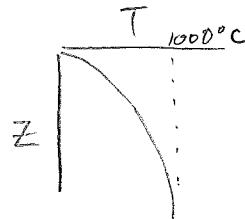
$$\frac{\Delta\rho}{\rho} \sim 3\%$$

thermal

consider a TBL

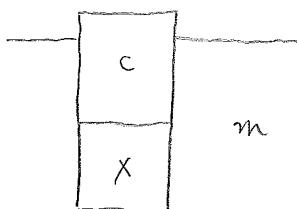
$$\Delta T \sim 500^\circ\text{C}$$

$$\alpha = 3 \times 10^{-5}/^\circ\text{C}$$



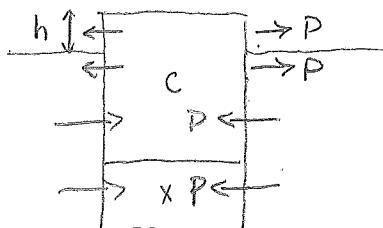
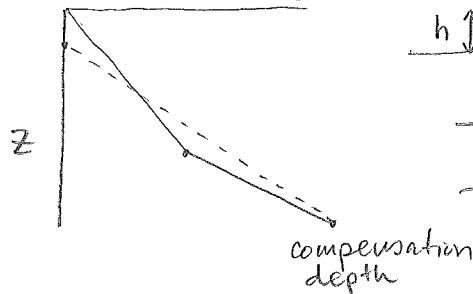
$$\frac{\Delta\rho}{\rho} \sim 1.5\%$$

So why are  $\rho$  (high  $\rho$ ) things negatively buoyant?



consider a crustal column made of felsic crust  $c$  and eclogite crust  $x$  with  $\rho_c < \rho_m$  (mantle)  
but  $\rho_x > \rho_m > \rho_c$

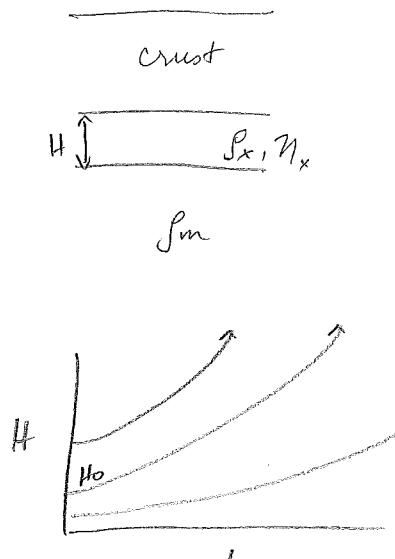
$$P = \int \rho g dz$$



- note that upper part gravitationally collapses.
- lower part,  $P$  pushes in which tries to force dense root off.

This dense root will come off if the downward buoyancy forces exceed viscous resistance.

- Let's assume that the dense layer is slightly colder than ambient mantle  $m$ . Then, the main viscous resistance comes from within the dense layer rather than from the surroundings



$$\Delta \rho = \rho_x - \rho_m$$

$$\Delta \rho g H \sim \gamma \dot{H} \sim \gamma \frac{dH}{dt} \frac{1}{H_0}$$

$$H = H_0 \exp\left(\frac{\gamma \Delta \rho g H_0}{\eta} t\right)$$

↑  
initial lengthscale

$\gamma$  is geometrical constant

$$t_{e-fold} = \frac{\eta}{\gamma \Delta \rho g H_0}$$

Rayleigh-Taylor approximation

if  $\Delta \rho = 0$ ,  $H_0 = 0$ ,  $\eta$  is high it takes too long to fall off

growth of instability aided if  $H_0$  large

$\Delta \rho$  large

$\eta$  small

NOTE: if  $\Delta \rho$  is thermal, then thermal diffusion competes

$$\frac{H_0^2}{K} \sim t_{th} \quad \text{if } t_{th} < t_{growth}, \text{ thermal anomaly } \Delta T \text{ and } \Delta \rho \text{ erased:}$$

This requires thickening rates to be fast.

$$t_{\text{efld}} \sim \frac{\eta}{\gamma \Delta g H_0} = \frac{\eta}{\eta_0 \alpha g \Delta T H_0}$$

?

consider thermal  
contrasts

$3 \times 10^3 \frac{1}{\text{kg/m}^2}$      $3 \times 10^{-5} \text{ /}^\circ\text{C}$      $10 \frac{\text{m}}{\text{s}^2}$      $\sim 10^\circ\text{C}$

assume  $H_0 \sim 10 \text{ km}$

then if  $\eta = 10^{19} \text{ Pa.s}$      $t = 1 \text{ My}$

$$\eta = 10^{20} \quad t \sim 10 \text{ My}$$

$$\eta = 10^{21} \quad 100 \text{ My}$$

For  $H_0 = 10^2 \text{ km}$ ,  $\eta = 10^{21} \text{ Pa.s}$      $t = 10 \text{ My}$

So viscosity is very important

$$\eta = \eta_0 \exp(+E_A/kT)$$

$$\eta(1400^\circ\text{C}) = \eta_0 \exp(+E_A/kT_{1673\text{K}})$$

$$\frac{\eta(T)}{\eta(1673\text{K})} = \exp\left(+\frac{E_A}{R}\left(\frac{1}{T} - \frac{1}{1673}\right)\right)$$

$$E_A \sim 300 \text{ to } 500 \text{ kJ/mol}$$

$$R = 8.314 \times 10^{-3} \text{ kJ/K mol}$$

$$\text{if } \eta_{1673} = 10^{18} \text{ Pa.s}$$

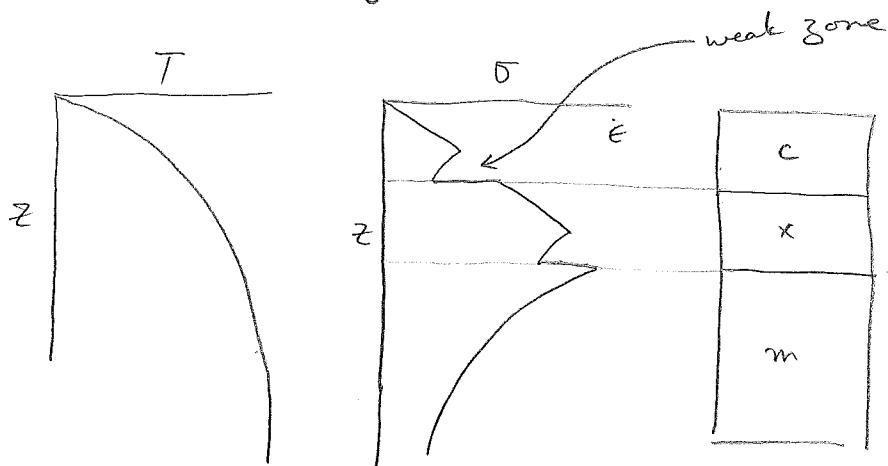
	$E_A = 300$	$E_A = 500$
$\eta_{1200\text{C}} = \eta_{1473\text{K}}$	$1.9 \times 10^{19}$	$1.3 \times 10^{20}$
$\eta_{1000\text{C}} = \eta_{1273\text{K}}$	$8.8 \times 10^{20}$	$8 \times 10^{22}$
$\eta_{800\text{C}} = \eta_{1073\text{K}}$	$1.7 \times 10^{23}$	$5 \times 10^{26}$

It can be seen that if the dense layer is too cold, it cannot founder viscously because  $\eta$  is too high.

$T < 1000^\circ\text{C}$ , no foundering!

Alternative is to delaminate

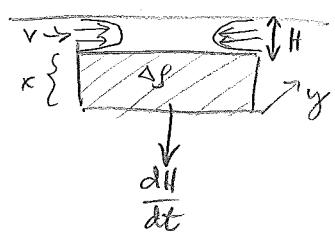
- here, dense layer is strong and detaches wholesale
- facilitated by a weak zone



- delamination can initiate along weak zone -
- weak zone in crust is enhanced when crust is thick

Model

assume lubrication theory



$$\Delta \rho g L x y = \eta \frac{V}{H} L y$$

buoy. force from dense  
slab

all viscous  
resistance  
controlled by  
flow in gap

$$\text{conservation of mass} \quad V \cdot H = \frac{dH}{dt} L$$

$$V = \frac{dH}{H dt} L$$

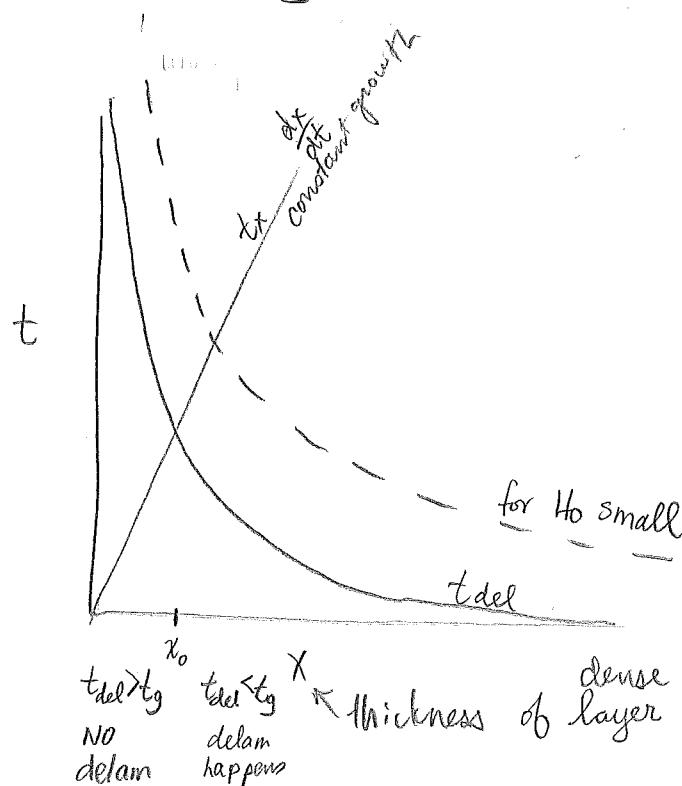
$$\text{plug in } \frac{\Delta \rho g H^2 X}{\eta L} \sim \frac{dH}{dt} \Rightarrow H = \frac{\eta L H_0}{\eta L - \Delta \rho g x t H_0}$$

$$t_{H_0} = \eta L / \Delta \rho g x H_0$$

rate of delamination scales with gap thickness to  $H^2$   
inversely to  $\eta$

$$t_{\text{delam}} = t_{H_0} = \frac{\eta L}{\Delta \rho g \times H_0} = \frac{\eta}{\Delta \rho g \times} \frac{L}{H_0}$$

- if gap is long and thin ( $L \gg 1, H_0 \ll 1$ )  
then  $t$  is long
- note also that  $t_{H_0} \sim \frac{1}{x}$  which is  
thickness of dense layer. If dense layer  
grows by magmatic underplating at rate  $\frac{dx}{dt}$   
then initially not unstable



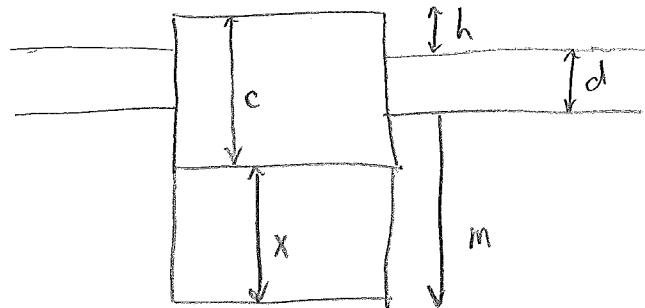
$x_0$   
 $t_{\text{del}} > t_g$     $t_{\text{del}} < t_g$     $x$    thickness of dense layer  
no delam happens

$x$  must grow to  $x_0$

$$x_0 = \sqrt{\frac{\eta}{\Delta \rho g} \frac{L}{H_0} \frac{dx}{dt}}$$

$x > x_0$  to delaminate  
 $x < x_0$  no delamination

Now, once the dense layer detaches, isostatic rebound will give rise to high elevations



$$h + d + m = c + x$$

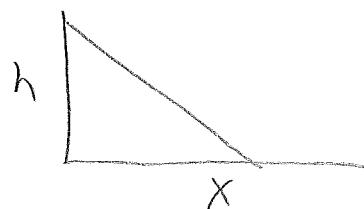
$$\rho_c c + \rho_x x = \rho_c d + \rho_m m$$

$$h = \frac{(\rho_m - \rho_c)c + (\rho_m - \rho_x)x + (\rho_c - \rho_m)d}{\rho_m}$$

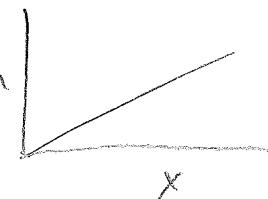
2nd term on RHS controls elevation  $h$  if everything else held constant

$$\frac{dh}{dx} = \left( \frac{\rho_m - \rho_x}{\rho_m} \right) \quad \begin{array}{l} \text{change in elevation due to} \\ \text{change in } x \text{ thickness} \end{array}$$

- if  $\rho_m - \rho_x < 0$   
decrease  $x$ , increases elevation



- if  $\rho_m - \rho_x > 0$   
decrease  $x \rightarrow$  decrease elev.  $h$

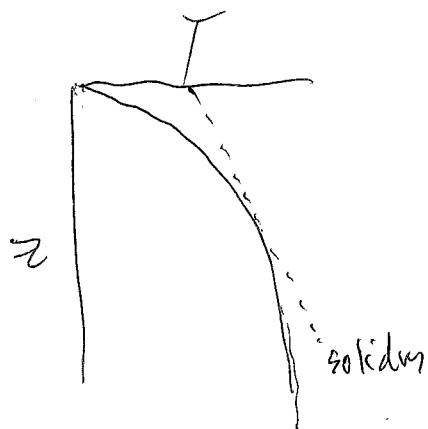


detachment of dense lower crust, if previously in isostatic balance, leads to uplift.

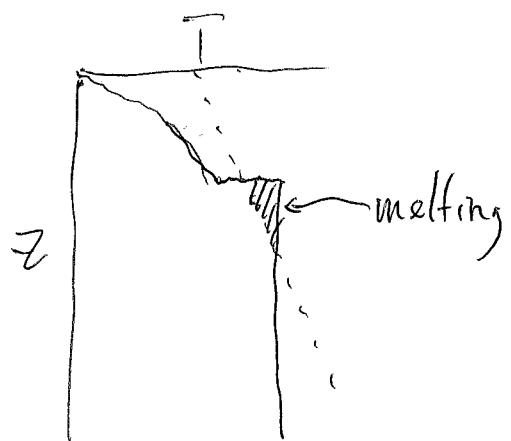
Note, the mantle  $m$  doesn't have to be anomalously hot.

What happens after delamination in terms of melting?

- delamination is fast (once it initiates) too fast for thermal re-equilibration (by diffusion)
- asthenosphere upwells in response



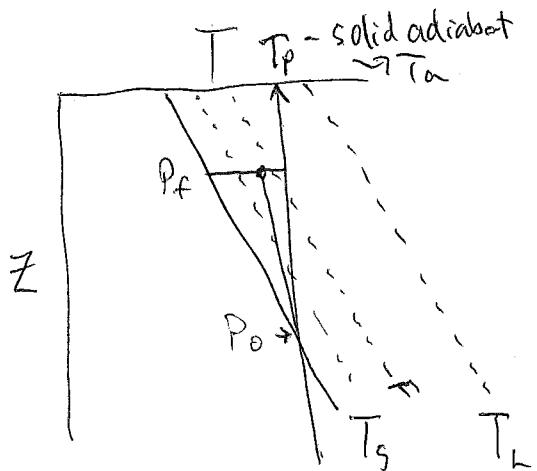
pre-delamination



after delamination

What is response in terms of melting?

from Langmuir (1992)



$$(P_f - P_0) \left[ \frac{dT}{dP_a} - \frac{dT}{dP_s} \right] = F \left[ \frac{H_f}{C_p} + \frac{dT}{dF} \right]$$

$$\frac{dF}{dP} = \frac{(dT/dP)_a - (dT/dP)_s}{H_f/C_p + dT/dF}$$

$$\frac{dT}{dF} = 3.5\% \quad \text{for } F < 0.22$$

$$\frac{dT}{dP_a} = 1^\circ C / kbar$$

$$\frac{dT}{dP_s} = 12^\circ / kbar$$

$$H_f = 100 \text{ cal/g}$$

$$C_p = 0.3 \text{ cal/g}^\circ K$$

Extent of melting depends on  $T_p$  and  $P_f$

$P_f$  limited by point of delamination.